

# Voltage Source Inverter Filter with Improved Proportional Gain for Dynamic Power and Melodies Mitigation in Three-Phase Three-Wire Distribution Systems

Parvesh Saini<sup>1</sup>, Sandeep Sunori<sup>2</sup>

<sup>1</sup>Department of Electrical Engineering, Graphic Era Deemed to be University, Dehradun, Uttarakhand India, 248002

<sup>2</sup>Department of Electronics & Communication Engineering, Graphic Era Deemed to be University, Dehradun, Uttarakhand India, 248002

---

## ABSTRACT

The purpose of this report is to examine the religious affiliations of High quality power is achieved by keeping the voltage on the distribution bus, which supplies most of the building, constant and at the specified frequency and magnitude. The creation of harmonics has a significant impact on this. Power quality may be diminished because to harmonic currents and excessive reactive power consumption by electronic and non-linear devices, despite their adaptability, low cost, and high efficiency. In order to adjust for a wide variety of nonlinear loads, researchers have investigated a family of distinct shunt hybrid active power filters in both shunt and series configurations. They increase the power factor and eliminate harmonic current by injecting current in a regulated manner at the source end of the electrical system. This study demonstrates how to improve a shunt active power filter to enhance power quality. The suggested subject features the use of a PI controller, a filter hysteresis current control loop, and a dc link capacitor. Using hysteresis current controller methods, the filter's switching signals are generated. Total harmonic distortion is reduced by this shunt active power filter's several elements. The PI control approach is implemented, and the resulting source current, compensatory current, and THD values are analysed. Beginning with the transfer function of the tiny signal system, the PI feedback compensation design is developed. Then, to improve the Shunt-responsiveness APF's to compensating harmonics of linear and non-linear loads, a suggested constant of PI is incorporated. Based on the findings, it is clear that present harmonic distortion may be mitigated by using compensation. The compensation speed of the outer loop that controls the dc bus voltage of the filter determines the magnitude of the voltage swings. The current harmonics are effectively compensated for by the suggested shunt active filter architecture, which employs a balanced linear and non-linear load. The harmonic in the source current is decreased thanks to the MATLAB/SIMULINK model.

**Keywords:** Voltage Source Inverter, Power quality, shunt active filter architecture.

---

## INTRODUCTION

Virtual Using MATLAB SIMULINK, we simulate a three-phase, three-wire Shunt Active Power Filter with optimum PI control techniques for balanced and unbalanced loads.

The p-q model

approach for immediate and consistent power regulation i. Sinusoidal current regulation technique  
Standardized Fryze current regulation approach

b) d-q theory The functionality of a shunt Active Power Filter under balanced and unbalanced loads is simulated here. Shunt passive filter performance is analysed using MATLAB SIMULINK for both balanced and unbalanced loads in a variety of scenarios, and the optimal design is determined by comparing the findings. 2. All simulation models have had their THD% and power factor calculated. Summary information is provided in this section. It begins with a literature review, then moves on to a short explanation of power quality, harmonic sources, and their impacts. In this section, I discuss the goals and structure of my thesis. The Nature of the Power in the Background

Any event exhibited in voltage, current, or frequency variations that causes damage, upset, failure, or mis-operation of end-use equipment is referred to as a power quality (PQ) problem. Every commercial, household, and industrial application has some kind of relationship with PQ problems. Home electronics like televisions and computers, office machinery like photocopiers and printers, and manufacturing tools like PLCs, ASDs, rectifiers, inverters, CNC machines, and so on all rely on power electronics. There are a variety of signs that indicate a Power Quality (PQ) problem, such as:

- lamp flickering
- frequent blackouts
- frequent dropouts in sensitive equipment

Unexpected grounding of voltage, interruptions in communications, and overheated components and machinery are all potential issues.

Harmonics, interharmonics, notches, and neutral currents may all be traced back to PE. Rectifiers, automatic voltage regulators (VRs), automatic switching power supplies (APS), soft starters, electronic ballasts for discharge lights, and air conditioning and refrigeration with APS all contribute to harmonics in the electrical system. Transformers, motors, cables, interrupters, and capacitors are just some of the devices that might be negatively impacted by harmonics (resonance). Generally speaking, notches are generated by converters and primarily impact electronic control devices. Computers, printers, photocopiers, and any other generator that uses a switched-mode power supply all contribute to the noise floor by creating neutral currents. As a result of neutral currents, the neutral conductor heats up and the transformer's output power is reduced significantly. Static frequency converters, cyclo-converters, induction motors, and arcing devices all generate inter harmonics.

Depending on the nature of the equipment and the source of the disturbance, various degrees of sensitivity to PQ problems may be seen. As for the impact of PE on the PQ of electric power systems, it varies according on the specific kind of PE being used. In terms of overall harmonic distortion, the IEEE standard specifies the maximum allowable levels of harmonic contamination.

Power electronics continue to thrive in practical applications, where they are used to solve the issues that plague distribution networks. There are three sides to power electronics: one that brings useful

appliances into the home and workplace, another that causes difficulties, and a third that contributes to their resolution. One way in which power electronics and microelectronics have improved the quality of contemporary living is by facilitating the spread of high-tech, easily-controllable appliances in both commercial and domestic settings. On the other hand, these delicate technologies are causing friction between each other, which is making it harder to maintain quality of service in electric energy supply and costing customers billions of dollars in lost productivity. Fixing the Issues with Our Power Supply

To reduce power quality issues, two methods may be used. The first strategy, termed load conditioning, involves making the equipment less vulnerable to power disturbances so that it may continue functioning despite high levels of voltage distortion. Installing line-conditioning equipment to minimise or counteract the power system disruptions is another option. Traditionally, harmonic currents in distribution systems have been regulated primarily by the use of passive filters. Typically, they are developed specifically for the task at hand. Their effectiveness is restricted to a small range of harmonics, and they have the potential to cause resonance in the electrical grid. Active power filters have shown to be an essential and adaptable alternative to correct for current and voltage disturbances in power distribution systems, among the many new technological solutions available to enhance power quality. Although the concept of active filters is not new, recent advancements in power electronics, microcomputer control systems, and the decreasing cost of electronic components have allowed for its practical implementation. Due to their decreasing price, active power filters are quickly replacing passive filters as a viable option. The active filter uses power electronics to provide new current or voltage that cancels out the harmonic components of nonlinear loads or supply lines. Numerous topologies for active power filters have been developed, and many of them are commercially available. Filters for Harmonic Currents

As non-linear demands on the power supply network continue to rise, concerns have been voiced concerning the network's capacity to provide a consistent and high quality of electricity. The difficulty is in determining how and where to use harmonic filters for optimal performance. In this chapter, we'll talk about the various non-linear loads and the filters that will be required to successfully reduce harmonics in the system. Input Voltage Non-Linear `

A static compensator (STATCOM) is often used for reactive power compensation in power transmission systems, and the shunt-connected active power filter with a self-controlled dc bus has a topology very similar to that of a STATCOM. By injecting a current that is identical in magnitude but opposite in phase to the load current, shunt active power filters may neutralise the negative effects of harmonics in the latter. In this configuration, the shunt active power filter acts as a current source, injecting the phase-shifted (180 degrees) harmonic components produced by the load [1].

In this case, the PI controller is the recipient of the error signal. The maximum value of the reference current has been taken as the output of the PI controller. The reference currents ( $i_{sa}^*$ ,  $i_{sb}^*$ , and  $i_{sc}^*$ ) are then calculated by multiplying this value by the unit sine vectors ( $u_{sa}$ ,  $u_{sb}$ , and  $u_{sc}$ ) that are in phase with the source voltages. The PWM converter's switching signals are generated using reference and real currents fed into a hysteresis-based, carrier-free PWM current controller[2]. How switches behave is determined by the delta between the reference current template and the actual

current. By turning on the top switch of a phase's PWM converter, that phase's current may be reduced, while turning on the bottom switch increases the current [3]. After being amplified and isolated, these switching signals are sent to the relevant equipment. In order to offset the load's harmonic current and reactive power, the current passes through the filter inductor  $L_c$  as a result of the switching operations [4].

### **The Simulation and Implementation**

Requirements for shunt APF system design 5.1: Power factor, or  $V_{ph}$ , = 100 (rms value).

Measurement of source impedance:

$R_s = 3.6 \Omega$ .  $L_s = 5.8 \mu H$ .

$F_s = 50$  Hz is the frequency of the power supply.

The settings of the compensator:

$V_{dc} = 210$  V.

$C_{dc} = 40 \mu F$ .  $L_f = 1.2$  mH.

Load factor  $RL=25$  indicates standard operation.  $I_L=55$  mA

$R = 10$  are the linear load parameters.

Parameters for a non-linear load:  $R = 25$ .

$L = 12$  mH.  $C = 2200 \mu F$ .

Due to the lack of a common or neutral wire in this model's three-wire layout, zero-sequence current components are absent. This means that the source current is neither symmetrical or sinusoidal.

$Z_t$  is implemented due to the PWM current controller's utilisation of a force inverter to imitate a regulated current source. Shunt APFs must be coupled to loads via inductors  $Z_t$ , also known as commutation inductors, to prevent excessive inductive kick; circuit breakers are used to operate APFs with a 0.02-second delay to account for before and after compensation effects and to prevent negative sequence currents from being wiped out altogether if all imaginary power is compensated [5].

Because there is no neutral, zero-sequence power in this system, only active and reactive power exist, according to  $P_q$  theory. The 10 ohm resistor in the DC sector is used to restrict or compensate for reactive power [6].

PCC uses a different circuit breaker, this one having a 0.01% delay in operation. This implies that the shunt APF is connected to the system after 0.01, and the circuit breaker is closed. Since the APF isn't active between  $t=0$  and  $t=0.01$ , the waveform must be significantly skewed throughout that interval. On the other hand, I see that the waveform's basic characteristics remain constant regardless of context [9].

After 0.02 seconds of adjustment, the source current is a pure sinusoid with a 3.02% THD at 50 Hz, therefore the active power filter is activated. Since all fictitious power would be compensated, negative sequence currents would be eliminated if the circuit breakers were not programmed to run APF with a 0.02-second delay [10]. Since positive sequence current is responsible for active power transmission to the load, its nature would not change.

With the transition to 50 Hz as the new operating frequency, we have set the upper frequency limit to 100 Hz. Furthermore, we have a time range of 0.02 to 2.0, with an unchanged positive current from our APF, which works at 0.02. It's in my best interest to check this out. If you want to experiment with the waveform display, you may test out ten different cycles (here 0.2 so put initial time 0.0 so on) [7]. The steady-state inaccuracy is eliminated by using a Pi controller. Here,  $V_{dc}$  must be monitored against  $V_{ref}$  to ensure it remains stable. In this case, a positive Ploss signal would be generated if  $V_{dc}$  (less than 100v) was less than  $V_{ref}$  (220v). A negative Ploss signal would be produced. A 5th order Butterworth filter with a cutoff frequency of  $2\pi \cdot 50$  is realised using an analogue filter. This is used to isolate the portion of the active power transfer that is not attributable to the underlying current. Connection inductors are used to connect a power inverter to a point of common coupling (PCC). Its purpose is to reduce the impact of  $L_{di}/dt$  [8]. This compensating current is generated by discharging DC capacitors via the inverter. When this happens, the harmonics are produced by the capacitors rather than the original source. Non-linear Unbalanced Load: • We attempted to employ an Instantaneous technique here in which just the active avg. real from the load is used and the rest power is wasted (from harmonics is exchanged with shunt APF). The shunt APF operates in a closed-loop system, continually sampling the load current and deriving the compensating current as reference  $i^*c$  for the PWM converter.

In the case of a pure resistive unbalanced load, the presence of constant instantaneous active power is attributable to the positive sequence current, and in the case of an inductive or capacitive unbalanced load, the presence of constant imaginary power is attributable to the positive sequence current. In both circumstances, oscillations are produced by the presence of negative sequence current.

To restrict the negative sequence current produced by the capacitive load, a 10 ohm resistor has been connected.

Three independent single-phase diode rectifiers feeding a parallel RC-load with variable values on each phase constitute a nonlinear unbalanced load.

In which  $R_1 = 16.67$  and  $C_1 = 2200F$ ;  $R_2 = 25$  and  $C_2 = 2200F$ ; and  $R_3 = 50$  and  $C_3 = 2200F$ .

To combine the before- and after-compensation effects, the APF is programmed to function with a 0.02-delay using circuit breakers and a PCC for selective compensation features.

## **RESULTS**

Result From Waveforms:

Having an imbalanced load causes a negative sequence current, which causes power fluctuations. In the case of a purely resistive load, although this may be unbalanced, the presence of constant instantaneous active power is due to the positive sequence current. In the case of a pure inductive load, but perhaps an unbalanced one, the appearance of a constant instantaneous imaginary power is caused by the positive sequence current. Whether a load is entirely resistive or inductive, the appearance of oscillations in both of the instantaneous powers is attributable to the negative sequence current.

### Results of FFT analysis

Assuming the value of PI is 210. Technically, a THD of 5.52% is well within the allowable range, as stipulated by IEEE 519 harmonics limit for the balanced load situation. According to IEEE 519, the maximum allowable total harmonic distortion (THD) for an unbalanced RC load is 3.05%. Technically, the THD of an unbalanced RLC load is 6.41 percent, which is well within the tolerance range specified by IEEE Standard 519 for harmonics. According to IEEE 519, the maximum allowable total harmonic distortion (THD) for an unbalanced RLC load situation is 7.25 percent.

### CONCLUSION

In the case of a purely resistive load, although this may be unbalanced, the presence of constant instantaneous active power is due to the positive sequence current. For pure inductive loads, but perhaps unbalanced loads as well, the occurrence of constant instantaneous imaginary power is attributable to the positive sequence current. Whether a load is entirely resistive or inductive, the appearance of oscillations in both of the instantaneous powers is attributable to the negative sequence current. Based on the results of the FFT analysis and the tables 1–4, it seems that the suggested shunt-APF system with the optimised PI system along constant 210 provides the best power factor solutions for both balanced and unbalanced configurations of load (R, RC, RL, and RLC).

### REFERENCES

1. Judewicz, M. G., González, S. A., Fischer, J. R., Martínez, J. F., & Carrica, D. O. (2018). Inverter-side current control of grid-connected voltage source inverters with LCL filter based on generalized predictive control. *IEEE Journal of Emerging and Selected Topics in Power Electronics*, 6(4), 1732-1743.
2. Schiesser, M., Wasterlain, S., Marchesoni, M., & Carpita, M. (2018). A simplified design strategy for multi-resonant current control of a grid-connected voltage source inverter with an LCL filter. *Energies*, 11(3), 609.
3. Tahir, S., Wang, J., Baloch, M. H., & Kaloi, G. S. (2018). Digital control techniques based on voltage source inverters in renewable energy applications: A review. *Electronics*, 7(2), 18.
4. Nazeri, A. A., Zacharias, P., Ibanez, F. M., & Somkun, S. (2019, June). Design of proportional-resonant controller with zero steady-state error for a single-phase grid-connected voltage source inverter with an LCL output filter. In *2019 IEEE Milan PowerTech* (pp. 1-6). IEEE.
5. Li, H., Zhang, X., Shao, T., & Zheng, T. Q. (2018). Flexible inertia optimization for single-phase voltage source inverter based on hold filter. *IEEE Journal of Emerging and Selected Topics in Power Electronics*, 7(2), 1300-1310.
6. Lee, J. Y., Cho, Y. P., Kim, H. S., & Jung, J. H. (2018). Design methodology of passive damped LCL filter using current controller for grid-connected three-phase voltage-source inverters. *Journal of Power Electronics*, 18(4), 1178-1189.
7. Gomes, C. C., Cupertino, A. F., & Pereira, H. A. (2018). Damping techniques for grid-connected voltage source converters based on LCL filter: An overview. *Renewable and*

Sustainable Energy Reviews, 81, 116-135.

8. Albatran, S., Koran, A., Smadi, I. A., & Ahmad, H. J. (2018). Optimal design of passive RC-damped LCL filter for grid-connected voltage source inverters. *Electrical Engineering*, 100(4), 2499-2508.
9. Bai, H., Wang, X., Blaabjerg, F., & Loh, P. C. (2018). Harmonic analysis and mitigation of low-frequency switching voltage source inverter with auxiliary VSI. *IEEE Journal of Emerging and Selected Topics in Power Electronics*, 6(3), 1355-1365.
10. Gui, Y., Xu, Q., Blaabjerg, F., & Gong, H. (2019). Sliding mode control with grid voltage modulated DPC for voltage source inverters under distorted grid voltage. *CPSS Transactions on Power Electronics and Applications*, 4(3), 244-254.